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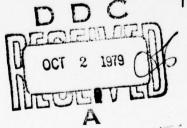
SPECTRAL, FAR-FIELD, AND NEAR-FIELD MEASUREMENTS OF FIVE LIGHT-EMITTING DIODES

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CR Zeisse SA Miller

JULY 1979

Test and Evaluation: April 1979 — May 1979



Prepared for Naval Air Systems Command

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The report presents results of near-field, spectral, and far-field meas emitting diodes selected at random from 45 manufactured by Laser Diodes.	surements performed on 5 light				

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INTRODUCTION

During the week of April 16, 1979, 45 light-emitting diodes (LEDs) were received at the Naval Ocean Systems Center (NOSC) from Laser Diode Laboratories, Incorporated. These diodes were produced under manufacturing technology contract number N00123-78-C-05700 for the purpose of improving LEDs for fiber bundle applications. Out of the diodes received, 5 were selected at random for further evaluation and assigned device serial numbers as follows:

Laser Diode Laboratory Number	Naval Ocean Systems Center Device Serial Number	Notation for Figures and Tables in this Report
5	DSN118	a
15	DSN119	b
25	DSN120	c
36	DSN121	d
40	DSN122	e

Near-field, spectral, and far-field measurements (in that order) were then performed on each of the 5 diodes. A thin aperture, 0.045 inch in diameter, was centered on the face of each diode for the far-field and near-field measurements. During the beginning of the spectral measurement for DSN121, the diode open-circuited while 100 mA of current was flowing through it. Hence only near-field measurements appear for DSN121.

The purpose of this report is to present the results of these measurements, which were completed May 24, 1979. The measurements are presented in the following order: (1) spectral, (2) far-field, (3) near-field. A brief paragraph describing the measurement method and purpose begins each section. To facilitate the visual presentation of the data, the figures are not presented in the usual numerical order.

SPECTRAL MEASUREMENTS

The purpose of these measurements is to determine the relative spectral radiant power of the LED. To do this, the diode is driven with direct current and the radiant flux is focused with mirrors onto the entrance slit of a Jarrell-Ash 0.5-meter grating monochromator. The monochromatic light leaving the exit slit is focused onto an RCA model 30809 silicon photodetector. The optical beam is chopped at 20 Hz by a mechanical chopper in front of the entrance slit, and the resulting ac signal in the detector is amplified, rectified by a lock-in, digitized, and stored in computer memory as the raw data file for that particular diode. The raw data file is then corrected to take into account spectral variations not associated with the source and to adjust the wavelength marker from its nominal to true value.

Figures 1(a), (b), (c), and (e) show the relative spectral radiant flux $\Lambda(\lambda)$ and its integral with respect to wavelength for all diodes except (d), the one that developed an open circuit. The flux has been normalized so that its integral with respect to wavelength equals unity. Each diode was operated at 100 mA dc and the optical resolution was always better than 0.13 nm. Data were taken at 2-nm intervals.

Tables 1(a), (b), (c) and (e) present the data of figures 1(a), (b), (c), (d) in tabular form. The peak wavelength is the wavelength at which the spectral flux is a maximum. The average wavelength separates the spectrum into two equal areas: half the total flux lies at shorter wavelengths, and half the total flux lies at longer wavelengths. The spectral width is defined as the full width of the peak at half of its maximum value.

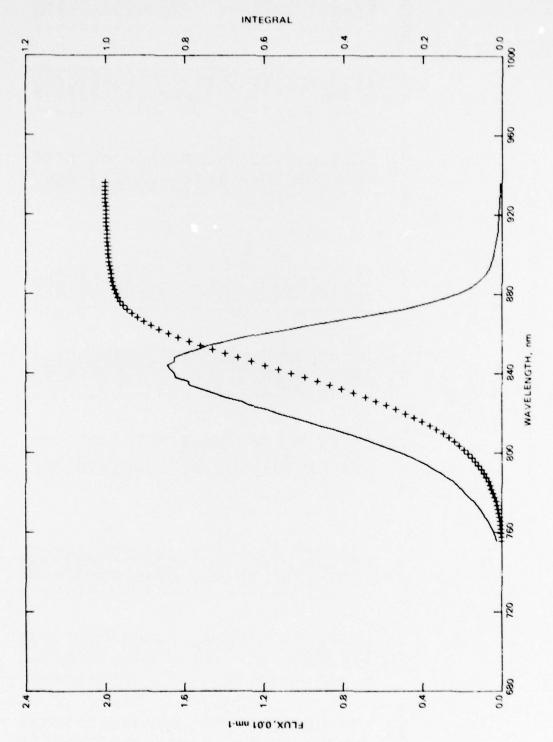


Figure 1(a). DSN118 S00.

Table 1(a). Relative spectral flux. Raw data file: DSN118.500.

ξ

838.88 84.38

ξ

844.00

PERK WAVELENGTH: AVERGCE WAVELENGTH: SPECTRAL WIDTH (FWHM):

INTEGRAL		0.00135	0.00464	0.00997	0.0180E	0.02958	0.04547	9.06709	98586	0.13391	0.18292	0.24401	0.31772	0.40322	0.49830	0.59847	0.69758	60.8887.0	86338	0.91864	0.95330	9.97266	98286	9.38856	6 99209	0.39458	6.99639	93764	8.99862	0.99934	8.99985	
AL X	(N=1)	0.00042	89000	0.00108	0.00162	0.00223	0.00307	0.00412	0.00551										0.01083													
LAVELENGTH	E C	22.73				783.83																										
INTEGRAL		0.00060				0.02531																										
7. X.	() = 1)	0.00034			-	0 00202							*	- 10	*					0.80	*	191				10.					0.000007	
MAYELENGTH	E	22.72						- 0.	*											-		-										
INTEGRAL		0.00000	0.00225	0.00616	0.01231	0.02146	0.03431	0.05200	0.07575	0.10749	0.14893	0.20190	0.26718	0.34497	8 4340E	0.53131	0.63186	0.72911	9.81526	0.88416	0.93238	9.96110	0.97682	0.98513	88388	8 39302	93256	83888	8.99799	6.39889	0.99954	1.00000
Ä		9.999SE	0.00048	0.00084	0.00124	0.00183	0.00250	0.00343	0.00453	0.00607	0.00785	9.99979	0.01185	0.01395	0.01572	0.01651	0.01653	0.01536	0.01313	0.00384	0.00636	0.00353	80184	0.00103	9.90961	0.00043	0.00031	0.000c1	0.00017	0.00013	8.88889	0.0000
UPVEL ENGTH	E C	82.35																		-											936.15	

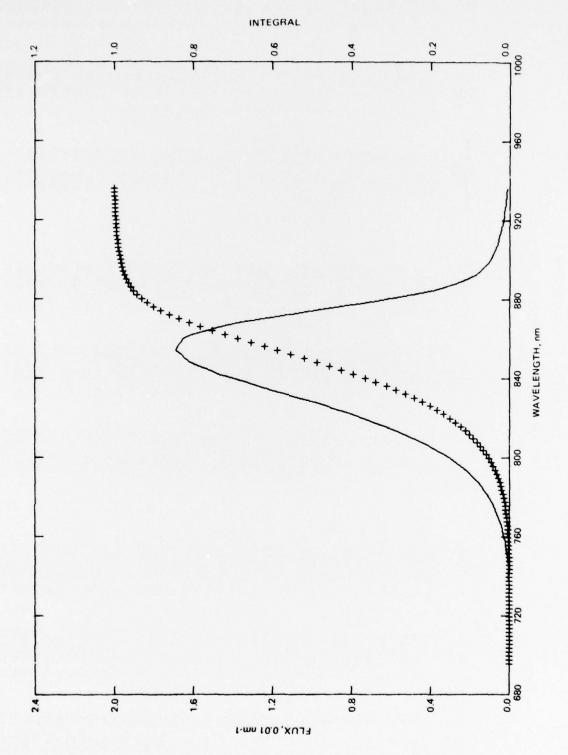


Figure 1(b). DSN119.S00.

Table 1(b). Relative spectral flux. Raw data file: DSN119,S00.

PERK WAVELENGTH:

AVERAGE WAVELENGTH: SPECTRAL WIDTH (FWHM):

854.82 M 848.74 M 53.44 M

INTEGRAL.	9.99993 9.99916 9.99915	0 000020	0 00034	0 000041	0 00081	0.00143	6.00263	0.00470	2000	200		0.04117	-			0.15216				0.42515	*	0.62190		0.81036						0.98814	0.99207	8.39493	0.39784	0.99857	0.99967	
₹ 1-1-1	9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	0 99901	0.00001	0 000001	0.000007	0.00015	0.00027	0.00040	20000	2000		0 00246	-	1.00			- 7			- 7	-		0.01607	- 91					-		-		*	0 00021	0.00016	
LAVELENGTH (NM)	699.78 85.78 87.11.7											1. 16		160	- 2	-	-	-			-		-	-				-	~					-		
INTEGRAL	9.99992 9.99993 9.99914	0.00018	0.00032	0 0000 00000 000000 000000	0.00069	0.00117	*	*		2010.0						- "				0.39512	0.48805	0.58735	0.68773	8,18	2.85846	0.91698	8.95133	9.96994	9.38916	0.98651	68066	0.99407	0.99641	0.99811	8.99934	
₹ 2-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.00000	0 00001	000000	0 00000	0 00011	0.00021	0.00037	*	2020		8 88552		0.00403	0.00534	0.00687	0.00872	0.01069	0.01274	0.0147E	*	-	0.01653	100		-		40	6.		-	0.00045	-	0 00000 4	0 00017	
MAVELENGTH (MY)	697.79 87.78 87.88 87.88															1.00					-			-	-	780						-	-	-	-	
IMTEGRAL	8 98888 8 98887 8 98818	0.00017	6.88829	8.99935	090000	0.00097	0.00177	8.88322	0.00200	0.00903	0.06193	0.03223	0.04633	0.06550	9.99195	0.12462	9.16767	0.22177	9.25736	0.36631	0.45600	0.55387	0.65458	6.75185	83993	0.000.0	0.94213	0.36495	9.37731	0.38467	9.38369	9,99313	0.33570	93256	8,99898	JEERE O
¥ 1.15	9 98888 9 98888 9 98888	0 000001	6 98861	9 90001	98884	6 99969	8 98018	8 88832	848848	20100	0.00145	0 00001	0.00270	696969	0.00487	8 8863E	80803	0.00000	0.01207	0.01335	0.01563	0.01660	8.01662	0.01230	0.010	2000	9.00511	0.0027	0.00153	0.00037	0 00000	030000	0 00037	9.99987	0.00019	6.00014
LIPARELENGTH (NM)	885.78 861.78 86.78																																			

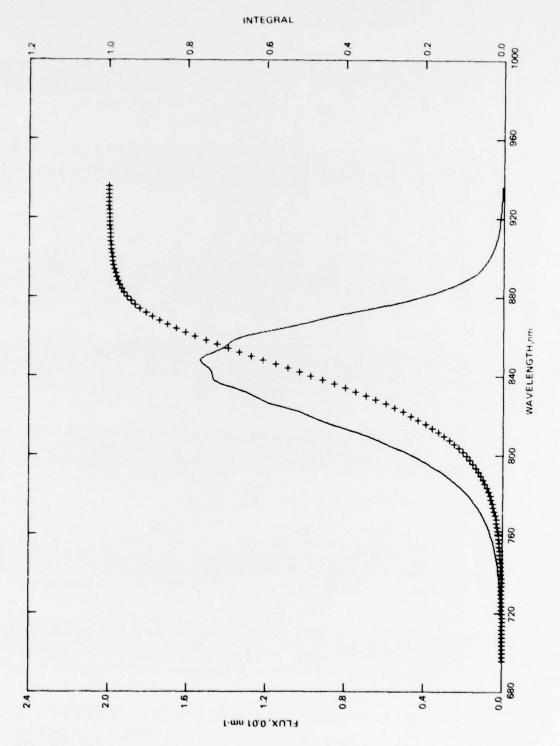


Figure 1(c). DSN120.S00.

Table 1(c). Relative spectral flux. Raw data file: DSN120.S00.

848.01 NM 840.86 59.72

PEAK WAVELENGTH:

ξ Z

SPECTRAL WIDTH (FWHM): AVERAGE WAVELENGTH:

INTEGRAL	9.98911 9.98933 9.98987 9.98987	8 8 8 1 8 7 8 8 8 8 8 8 8 8 8 8 8 8 8 8	6 6 6 1 5 1 5 6 6 6 6 6 6 6 6 6 6 6 6 6		6.54787 6.54659 6.54781 6.91938 6.95178	6 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9
FUK 11.		0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0			0 0 0 1 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	6 96913 6 96885 6 96856 6 96815 6 96611
URVELENGTH (NM)					888 888 865 8 888 865 8 888 865 8 888 866 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	
INTEGRAL	9 98885 9 98825 9 98849 9 98849	0 00113 0 000166 0 00333 0 00333			2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	* * * * * * * *
FLUX (NPT-1)	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0			20000000000000000000000000000000000000	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
URVELENGTH (NM)					28 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	
INTEGRAL	0.00000 0.00018 0.00011 0.00067	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	6 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	6 48787 6 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
FULK (NPT-1)	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 00317 0 0 00419 0 0 00548 0 0 0 00889 0 0 1036 0 0 1288	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
WAVELENGTH (NM)					28 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	

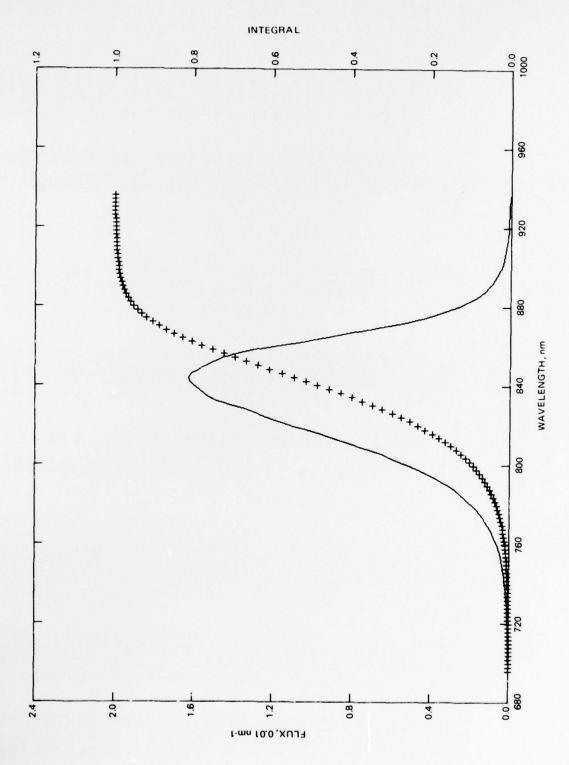


Figure 1(e). DSN122.S00.

Table 1(e). Relative spectral flux. Raw data file: DSN122.S00.

PERK WAVELENGTH:

AVERACE WAVELENGTH: SPECTRAL WIDTH (FWHM):

84.88 84.88 8.73 8.73 8.73

IMEGRAL	0.00011 0.00033 0.00058 0.00058	88888187 88888187 88588187 88588		00110000000000000000000000000000000000	88888888888888888888888888888888888888
\$ G. F. C.	9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 1 7 9 9 9 1 7 9 9 9	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0			0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
HAVELENGTH (NM)	* * * *				88888888888888888888888888888888888888
INTEGRAL.	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6			6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6
₹ 11.	9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0			0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
WAVELENGTH (NM)					288 28 28 28 28 28 28 28 28 28 28 28 28
INTEGRAL	9.98988 9.98918 9.88641	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
A 11. 11.					0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
URVELENGTH (NT)					24 8 8 8 8 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2

FAR-FIELD MEASUREMENTS

The radiant flux emitted by an LED into the hemisphere in front of it varies from point to point on the hemisphere and often presents a pattern unique to the individual LED being measured. Two diodes that emit the same total flux could therefore contain markedly different amounts of flux within a cone of a given half-angle, θ , and would therefore couple different amounts of flux into an optical fiber with a given numerical aperture. The amount of flux actually contained within a cone of half-angle θ can be found from the far-field measurements presented in this section.

The far-field measurements consist of a record of the angular distribution of radiant intensity of each diode. These measurements are performed by holding the diode in a goniometer capable of obeying computer commands to move to a given position defined by polar angle θ and azimuthal angle ϕ . The geometry of the far-field goniometer is shown in appendix A. A calibrated detector is placed at a distance D far enough away from the LED so that the active area of the detector subtends a small solid angle (on the order of 10^{-3} sr) at the LED. With a dc current of 100 mÅ through the diode, and with the goniometer "on-axis" (θ and ϕ both zero), the absolute flux falling on the detector is measured by recording the dc signal $i(0^{\circ}, 0^{\circ})$ from the detector. Following this, the LED current is changed to a square wave at 10⁴ Hz (that is, the bias is chopped electrically) and the ac signal from the detector is rectified by a lock-in amplifier, digitized, and stored in computer memory as the first entry of the far-field pattern, $m(0^{\circ}, 0^{\circ})$. The goniometer then moves the diode to a new polar angle (2 degrees in this case) and records the second entry m(2°, 0°). The entire far-field pattern is automatically scanned in this manner by incrementing the polar angle from 0° to 90° in 2° steps and the azimuthal angle from 0° to 360° in $22\frac{1}{2}^{\circ}$ steps. The series of entries $m(\theta, \phi)$, when divided by the first entry $m(0^{\circ}, 0^{\circ})$, then represents the relative radiant intensity of the diode at each position on the hemisphere.

Figures 2(a), (b), (c), and (e) show a section plot of the relative radiant intensity of diodes a, b, c and e. In these plots, the line of the emitter axis $(\theta, \phi) = (0^{\circ}, 0^{\circ})$ points vertically upward, θ is measured in a positive sense from the emitter axis to the direction of observation, and ϕ is measured positive in a counterclockwise sense looking along the axis into the emitter. Figures 3(a), (b), (c), and (e) represent the same data in the form of a grey scale plot. In this plot, light areas are high intensity, dark areas are low intensity, constant azimuth lines are radial, and constant polar angle lines are circular. The coordinates for the grey scale plot are given in appendix B. These figures provide a contour plot superimposed on the grey scale representation. Each contour represents the locus of a level of constant radiant intensity.

The relative far-field pattern can be converted to an absolute one by using the on-axis dc measurement. A major assumption of this conversion is separability, namely that the spectral radiant intensity l_{λ} (θ , ϕ , λ) W sr⁻¹ nm⁻¹ can be written as the product of a purely angular function $\Theta(\theta, \phi)$ in sr⁻¹, a purely spectral function $\Lambda(\lambda)$ in nm⁻¹ and a single constant Φ in W: l_{λ} (θ , ϕ , λ) $\equiv \partial^2 P/\partial\Omega\partial\lambda = \Phi \cdot \Theta(\theta, \phi) \cdot \Lambda(\lambda)$.* This means that the spectrum is independent of the angle at which it is observed. A minor assumption is that ac operation of the diode does not alter the relative radiant intensity. That is, it is assumed that m(θ , ϕ)/m(θ ^o, θ ^o) $\equiv \Theta(\theta, \phi)/\Theta(\theta$ ^o, θ ^o). With these assumptions it can then be shown that the radiant intensity $l(\theta, \phi) \equiv \partial P/\partial\Omega$ in W sr⁻¹ is given by

^{*}P is the radiant flux in watts emitted by the diode.

$$\mathbf{I}(\theta,\phi) = \begin{cases} \frac{D^2 - i(0^\circ,0^\circ)}{\int R(\lambda)\Lambda(\lambda)d\lambda} & \begin{cases} \frac{m(\theta,\phi)}{m(0^\circ,0^\circ)} \end{cases} \end{cases}$$

In this equation, $A(\lambda)$ is the normalized spectral flux presented in the previous section and $R(\lambda)$ is the absolute response of the detector in A cm² W⁻¹. The first bracket is the total on-axis dc radiant intensity $\Phi \cdot \Theta(0^{\circ}, 0^{\circ})$, and the second bracket is the relative ac farfield pattern. The integral over solid angle can be performed in two steps, first over azimuthal angle ϕ and then over polar angle θ . The integral over ϕ determines a function $G(\theta)$ which we have called the polar radiant intensity:

$$G(\theta) \equiv \int_{0}^{2\pi} I(\theta, \phi) d\phi = \Phi \cdot \Theta(0^{\circ}, 0^{\circ}) \int_{0}^{2\pi} \frac{m(\theta, \phi)}{m(0^{\circ}, 0^{\circ})} d\phi$$

The meaning of this function is that $G(\theta) \sin \theta \ d\theta$ is the amount of flux contained between polar angles θ and $\theta + d\theta$. The solid lines in figures 4(a), (b), (c), and (e) are plots of $G(\theta)$ in mW deg⁻¹.

The integral of $G(\theta) \sin(\theta)$ over θ determines the total flux contained within a cone of half-angle θ . We have called this integral the conical radiant flux. It is shown in milliwatts in figures 4(a), (b), (c), and (e) by the string of crosses.

Tables 2(a), (b), (c), and (e) represent the data of figures 4(a), (b), (c), and (e) in tabular form. The hemispherical flux is the total flux emitted by the diode into the forward hemisphere. The half-flux angle is the half-angle of a cone dividing the total flux into two equal parts; half the flux lies inside this cone, and half lies outside this cone.

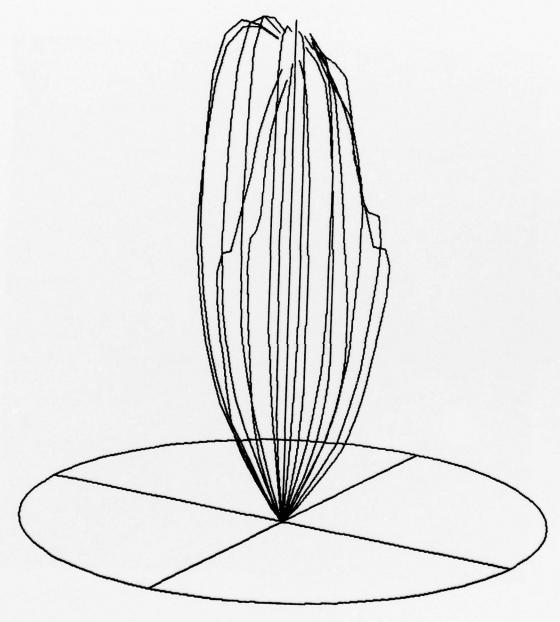


Figure 2(a). DSN118.FF4.

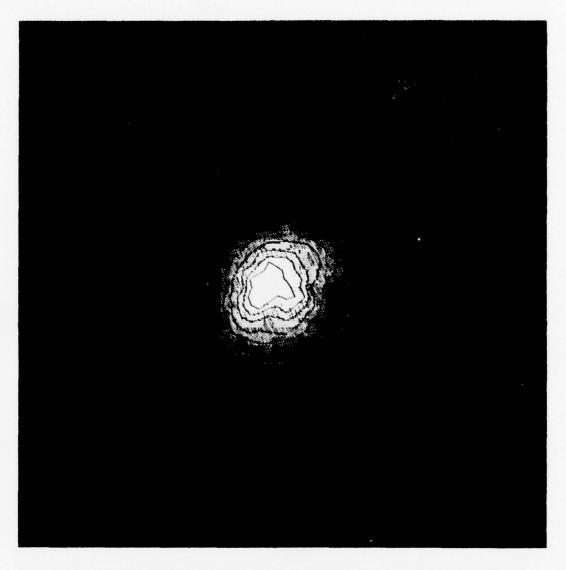


Figure 3(a). DSN118.FF4.

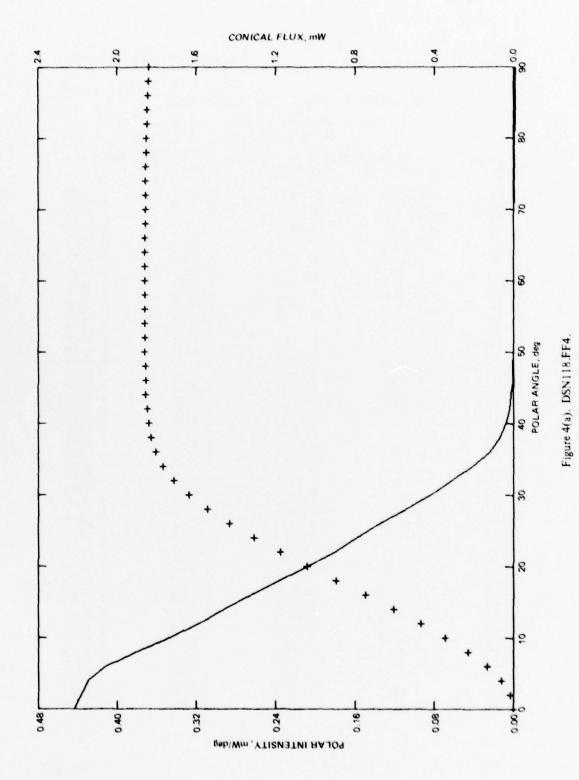


Table 2(a). Angular radiant intensity. Raw data file: DSN118.FF4.

HEMISPHERICAL FLUX:	1.839	MW
HALF-FLUX ANGLE	18.3	DEG

POLAR ANGLE	POLAR	INTENSITY (MU/RADIAN)	CONICAL F	·UK
(DEG)	(Dav DEG)			• •
0.00	442.9119	25.3770	0.0000	0.0000
2.00	436.5589	25.0130	0.0152 0.0604	0.0083
4.00 6.00	429.5601 411.1818	24.6120 23.5590	0.1334	0.0725
8.00	380.2372	21.7860	0.2293	0.1247
10.00	347.0934	19.8870	0.3425	0.1863
12.00	317.0214	18.1640	0.4687	0.2549
14.00	291.7490	16.7160	0.6051	0.3291
16.00	264.9757	15.1820	0.7488	0.4073
18.00	236.1778	13.5320	0.8948	0.4867
20.00	207.1879	11.8710	1.0386	0.5649
22.00	180.9905	10.3700	1.1773	0.6403
24.00	158.0796	9.0573	1.3094	0.7122
26.00 28.00	135.2681 108.5175	7.7503 8.2176	1.4330	0.7794 0.8393
30.00	84.0480	4.8156	1.6362	0.8899
32.00	62.6974	3.5923	1.7115	0.9309
34.00	41.7744	2.393\$	1.7680	0.9616
36.00	24.0349	1.3771	1.8055	0.9820
38.00	13.9120	0.7971	1.8282	0.9943
40.00	7.9973	0.4582	1.8419	1.0018
42.00	4.2579	0.2440	1.8499	1.0061
44.00	2.0672	0.1184	1.8542	1.0085
46.00	0.9750	0.0559	1.8563	1.0096
48.00 50.00	0.5238 0.3507	0.0300 0.0201	1.8574	1.0102
52.00	0.2404	0.0138	1.8585	1.0108
54.00	0.1557	0.0089	1.8589	1.0110
56.00	0.0896	0.0051	1.8591	1.0111
58.00	0.0395	0.0023	1.8592	1.0112
60.00	-0.0259	-0.0015	1.8592	1.0112
62.00	-0.0947	-0.0054	1.8591	1.0111
64.00	-0.1716	-0.0098	1.8588	1.0110
66.00	-0.2414	-0.0138	1.8585	1.0108
68.00	-0.3119	-0.0179	1.8579	1.0105
70.00 72.00	-0.3901 -0.4504	-0.0224 -0.0258	1.8573 1.8565	1.0102
74.00	-0.5419	-0.0310	1.8555	1.0092
76.00	-0.6682	-0.0383	1.8544	1.0086
78.00	-0.8445	-0.0484	1.8529	1.0078
80.00	-1.0104	-0.0579	1.8511	1.0068
82.00	-1.2162	-0.0697	1.8489	1.0056
84.00	-1.2867	-0.0737	1.8464	1.0042
86.00	-1.2970	-0.0743	1.8438	1.0028
88.00	-1.3104	-0.0751	1.8412	1.0014
90.00	-1.3208	-0.0757	1.8386	1.0000

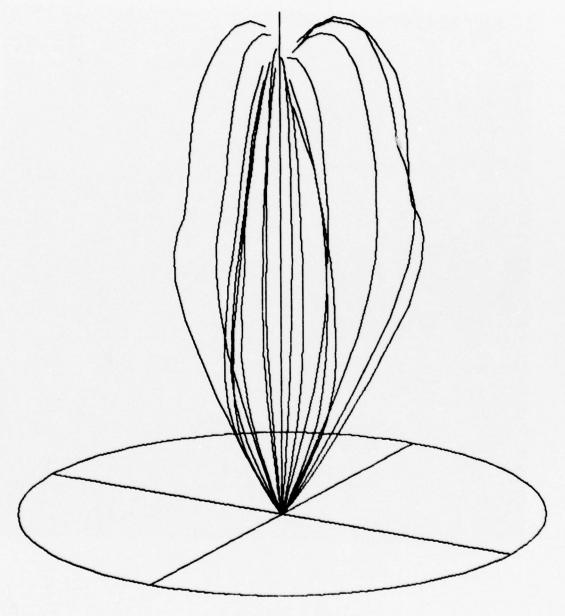


Figure 2(b). DSN119.FF3.



Figure 3(b) - "N119 FF3.

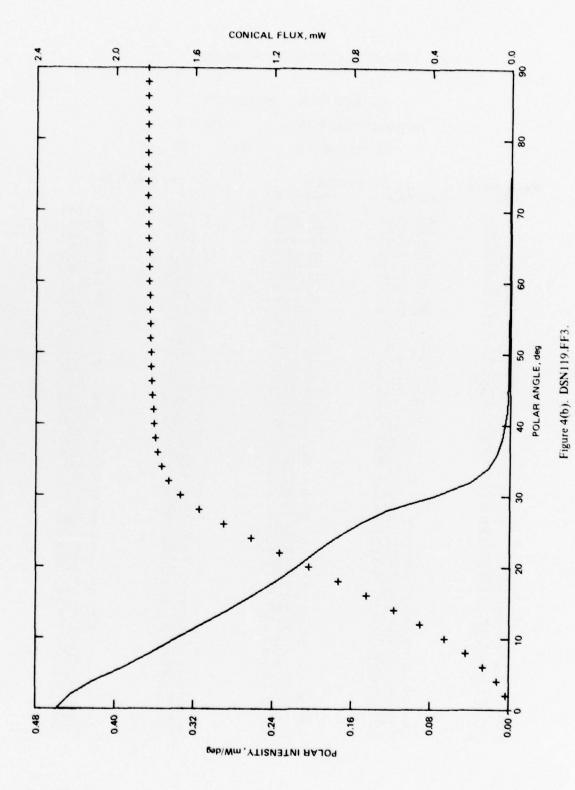


Table 2(b). Angular radiant intensity.

RAW DATA FILE: DSN119.FF3

HEMISPHERICAL FLUX: 1.839 MW

HALF-FLUX ANGLE: 18.7 DEG

POLAR ANGLE (DEG)	POLAR (UW/DEG)	INTENSITY (MU/RADIAN)	CONICAL	FLUX
DEG) 0.80 2.80 4.80 6.80 8.80 10.80 11.80 114.80 116.80 118.80 88.80	458.7420 444.2558 420.2051 388.1784 361.2654 335.6440 309.3070 283.3714 259.0939 236.4745 215.2862 196.4367 176.4527 172.8290 8.1697 128.8399 21.5792 12.8290 8.1699 5.2938 3.5085 2.5143 1.8398 1.5792 12.8290 8.1699 5.2938 1.5792 12.8290 8.1699 5.2938 1.5792 12.8290 8.1699 5.2938 1.5792 1.4301 1.3138 1.2106 1.1223 1.0392 0.9647 0.8818 0.7992 0.7384 0.6733 0.6001 0.5365 0.4659 0.3755 0.1253	(ML/RADIAN) 26.2840 25.4540 24.0760 22.2410 20.6990 19.2310 17.7220 16.2360 14.8450 13.5490 12.3350 11.2550 10.1100 8.7605 7.1177 4.4124 2.2826 1.2364 0.7351 0.4681 0.3033 0.2010 0.1441 0.1054 0.0931 0.0819 0.0753 0.0694 0.0693 0.0753 0.0694 0.0695 0.05553 0.0595 0.0595 0.0595 0.0595 0.0386 0.0386 0.0386 0.0387 0.0267 0.0215 0.0072	(MW) 0.0000 0.0155 0.0603 0.1302 0.2211 0.3296 0.4522 0.5851 0.7250 0.8695 1.0162 1.1635 1.3088 1.4476 1.5730 1.6698 1.7294 1.7626 1.7822 1.7948 1.8089 1.8130 1.8161 1.8186 1.8269 1.8230 1.8250 1.8250 1.8269 1.8250 1.8269 1.8250 1.8363 1.8374 1.8385 1.8374 1.8385	() 0.0000 0.0084 0.0328 0.0708 0.1202 0.1793 0.2460 0.3182 0.3943 0.5527 0.6328 0.7118 0.7873 0.8555 0.9682 0.9406 0.9587 0.9683 0.9762 0.9807 0.9807 0.9807 0.9901 0.9915 0.9916
80 00 82 00 84 00 86 00 83 00 90 00	-0.1036 -0.2164 -0.2306 -0.2327 -0.2401 -0.2350	-0.0059 -0.0124 -0.0132 -0.0133 -0.0138 -0.0135	1.8408 1.8405 1.8400 1.8396 1.8391 1.8386	1.0012 1.0010 1.0008 1.0005 1.0003 1.0000

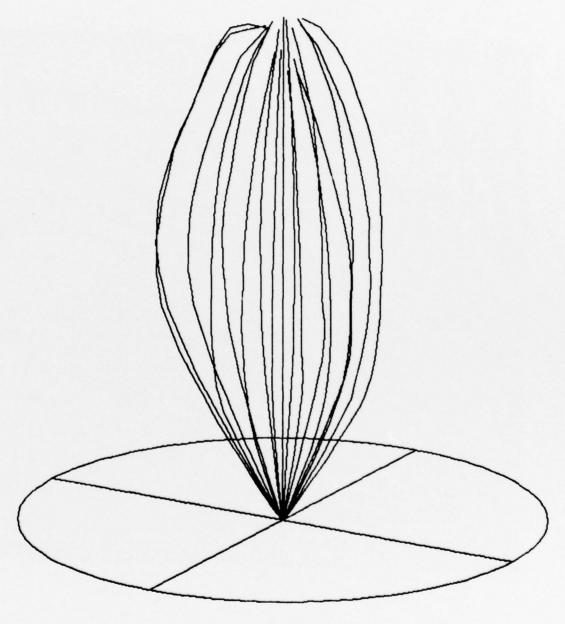


Figure 2(c). DSN120.FF3.

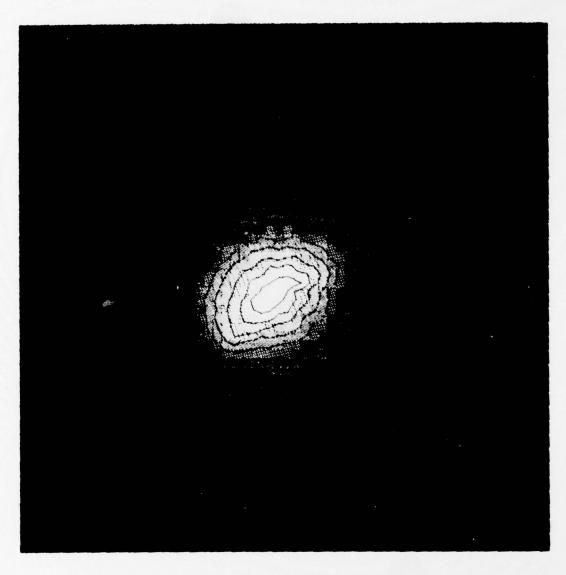


Figure 3(c). DSN120.FF3.

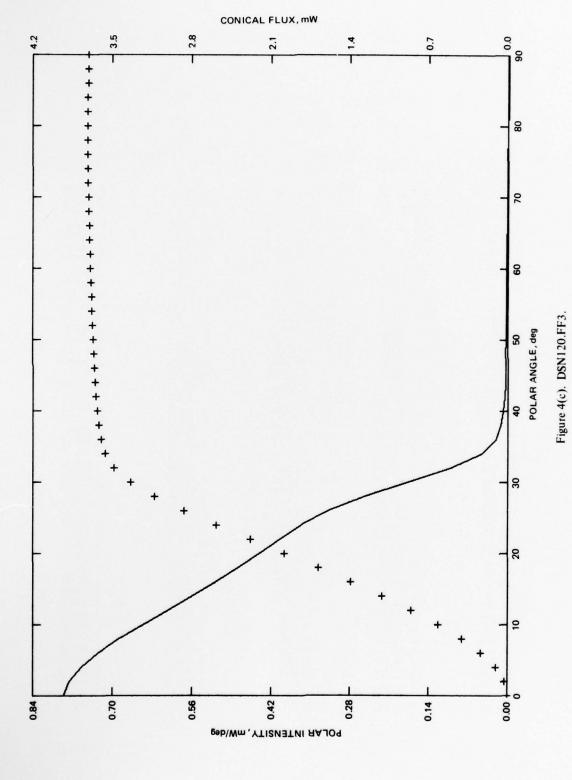


Table 2(c). Angular radiant intensity.

RAL DATA FILE: DSN120.FF3

HEMISPHERICAL FLUX: 3.708 MW
HALF-FLUX ANGLE: 19.2 DEG

POLAR ANGLE (DEG)	POLAR	INTENSITY (MW/RADIAN)	CONICAL	FLUX
0.00	785.3452	44.9970	0.0000	0.0000
2.00	775.4143	44.4280	0.0271	0.0073
4.00	754.4354	43.2260	0.1067	0.0288
6.00	724.6602	41.5200	0.2351	0.0634
8.00	689.0729	39.4810	0.4068	0.1097
10.00	645.4921	36.9840	0.6148	0.1658
12.00	601.6495	34.4720	0.8519	0.2297
14.00	559.7615	32.0720	1.1125	0.3000
16.00 18.00	517.3326 479.0052	29.6410 27.4450	1.39 0 5 1.6811	0.3750 0.4533
20.00	441.0793	25.2720	1.9800	0.5339
22.00	404.8114	23.1940	2.2825	0.6155
24.00	366.3618	20.9910	2.5831	0.6966
26.00	319.0808	18.2820	2.8720	0.7745
28.00	255.0971	14.6160	3.1317	0.8445
30.00	177.7093	10.1820	3.3403	0.9007
32.00	101.6776	5.8257	3.4830	0.9392
34.00	46.2477	2.6498	3.5628	0.9607
36.00	21.2668	1.2185	3.6011	0.9711
38.00	12.4363	0.7125	3.6213	0.9765
40.00	8.4038	0.4815	3.6343	0.9800
42.00	6.0870	0.3488	3.6438	0.9826
44.00	4.8443	0.2776	3.6513	0.9846
46.00	4.1938	0.2403	3.6576	0.9863
48.00	3.7884	0.2171	3.6635	0.9879
50.00	3.4880	0.1998	3.6690	0.9894
52.00	3.2552	0.1865	3.6742	0.9908
54.00	3.0367	0.1740	3.6792	0.9921
56.00	2.8421	0.1628	3.6840	0.9934
58.00	2.6815	0.1536	3.6887	0.9947
60.00 62.00	2.5230 2.3312	0.1446 0.1336	3.6931 3.6974	0.9959 0.9970
64.00	2.1256	0.1338	3.7013	0.9981
66.00	1.9181	0.1099	3.7050	0.9991
68.00	1.6800	0.0963	3.7083	1.0000
70.00	1.4454	8580.0	3.7112	1.0008
72.00	1.2555	0.0719	3.7138	1.0015
74.00	1.0489	0.0601	3.7160	1.0020
76.00	0.7257	0.0416	3.7177	1.0025
78.00	0.0578	0.0033	3.7184	1.0027
80.00	-0.5612	-0.0322	3.7180	1.0026
82.00	-0.9500	-0.0544	3.7165	1.0022
84.00	-1.0134	-0.0581	3.7145	1.0016
86.00	-1.0168	-0.0583	3.7125	1.0011
88.00	-1.0339	-0.0592	3.7104	1.0005
90.00	-1.0366	-0.0594	3.7084	1.0000

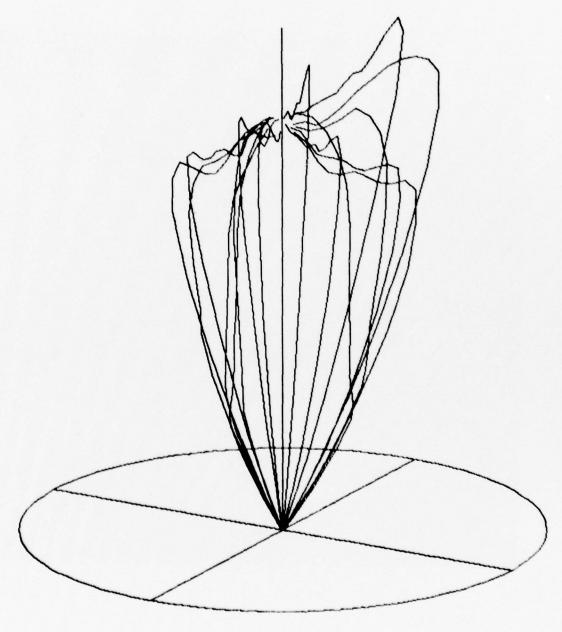


Figure 2(e). DSN122.FF2.

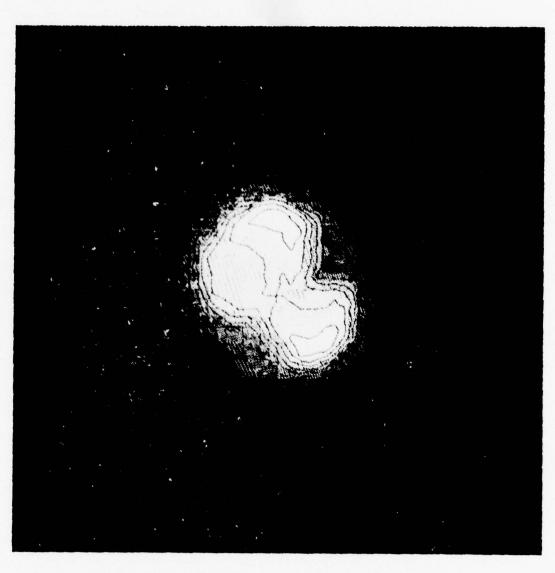
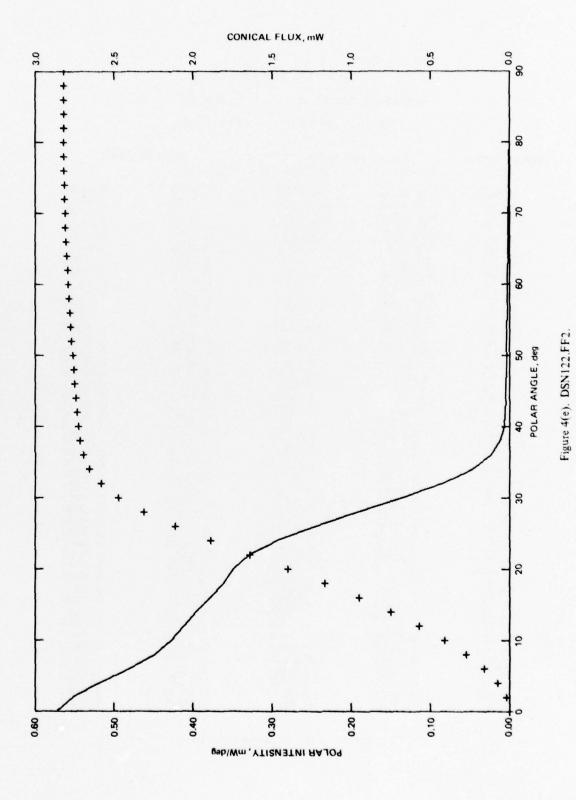


Figure 3(e). DSN122.FF2.



RAW DATA FILE: DSN122.FF2

HEMISPHERICAL FLUX:

2.819 MW

HALF-FLUX ANGLE:

20.1 DEG

POLAR ANGLE	POLAR	INTENSITY	CONICAL	FLUX
(DEG)	(UW/DEG)	(MW/RADIAN)	(MW)	()
0.00	573.0261	32.8320	0.0000	0.0000
2.00	552.3788	31.6490	0.0193	0.0068
4.00	517.7341	29.6640	0.0747	0.0265
6.00	479.5638	27.4770	0.1609	0.0571
8.00	447.9908	25.6680	0.2734	0.0970
10.00	426.7850	24.4530	0.4099	0.1454
12.00	410.9200	23.5440	0.5694	0.2020
14.00	395.7880	22.6770	0.7506	0.2663
16.00	378.2126	21.6700	0.9506	0.3372
18.00	361.4749	20.7110	1.1665	0.4138
20.00	348.9609	19.9940	1.3976	0.4958
22.00	328.8372	18.8410	1.6401	0.5818
24.00	294.0878	16.8500	1.8829	0.6680
26.00	245.5327	14.0680	2.1102	0.7486
28.00	193.2951	11.0750	2.3086	0.8190
30.00	136.6854	7.8315	2.4676	0.8754
32.00	85.8178	4.9170	2.5815	0.9158
34.00	46.6474	2.6727	2.6530	0.9411
36.00	23.8691	1.3676	2.6931	0.9554
38.00	11.8792	9.6806	2.7145	0.9630
40.00	7.1639	0.4105	2.7264	0.9672
42.00	5.6259	0.3223	2.7348	0.9702
44.00	5.0532	0.2895	2.7420	0.9727
46.00	4.6454	9.2662	2.7489	0.9752
48.00	4.3591	0.2498	2.7555	0.9775
50.00	4.1176	0.2359	2.7619	0.9798
52.00	3.8966	0.2233	2.7681	0.9820
54.00	3.7003	0.2120	2.7742	0.9841
56.00	3.4640	0.1985	2.7800	0.9862
58.00	3.2030	0.1835	2.7856	9.9882
60.00	2.9370	0.1683	2.7909	0.9901
62.00	2.6805	0.1536	2.7958	0.9918
64.20	2.4099	0.1381	2.8003	0.9934
66.00	2.1344	0.1223	2.8044	0.9949
68.00	1.9042	0.1091	2.8081	0.9962
70.00	1.6695	0.0957	2.8115	0.9974 0.9984
72.00	1.4166	0.0812 0.0685	2.8144 2.8169	0.9993
74.00	1.1948			1.0000
76.00	0.7780	0.0582 0.0446	2.8190 2.8208	1.0007
78.00 80.00	0.3807	0.0218	2.8219	1.0011
82.00	-0.1043	-0.0060	2.8222	1.0012
84.00	-0.1043	-0.0244	2.8217	1.0010
86.00	-0.4693	-0.0269	2.8208	1.0007
88.00	-0.4811	-0.0276	2.8198	1.0003
90.00	-0.4799	-0.0275	2.8189	1.0000
30.00	·	0.0073	L.0103	1.0000

Table 2(e). Angular radiant intensity.

NEAR-FIELD MEASUREMENTS

This series of measurements consists of a microscope scan across the glass window of the diode. The diode is mounted vertically on a pair of tables capable of translating the diode in 0.1-mil steps in the X and Y directions under computer control. The diode is excited with a 10⁴ Hz square wave. The optical radiation leaving the diode is collected with a 10 X 0.2 N. A. microscope objective and focused onto an 8-mil aperture in front of a silicon photodiode, defining a field of 0.8 mil in diameter at the LED window itself. The signal due to the flux from this field is sensed by a lock-in amplifier, digitized, and stored in computer memory. The tables are then stepped through a sequence of positions causing the diode to move through the stationary field. The entire operation is equivalent to the scan of an 0.8-mil photosensitive spot in the X and Y directions across the face of the diode window.

Near-field scans were performed with 1.0-mil steps in X and Y covering a 25-mil square.

The data from the near-field scans are presented from three different points of view. Figures 5(a) - (e) are perspective section plots in which intensity increases in the vertical direction. Figures 6(a) - (e) are contour plots showing lines of equal intensity superimposed upon a grey scale plot of the near-field data. Figures 7(a) - (e) are graphs whose ordinate is the amount of flux contained within a circle centered on the intensity centroid and whose abscissa is the diameter of the circle.

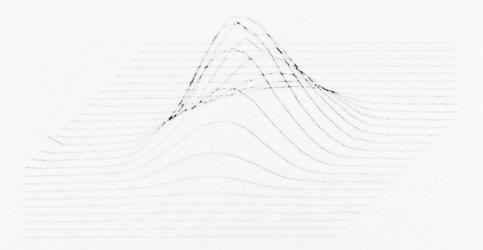


Figure 5(a). DSN118.NF1.

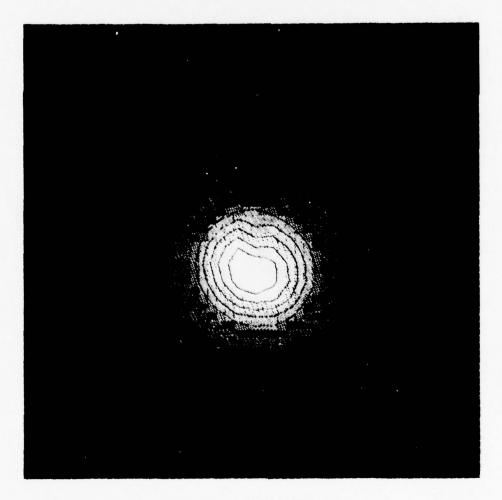
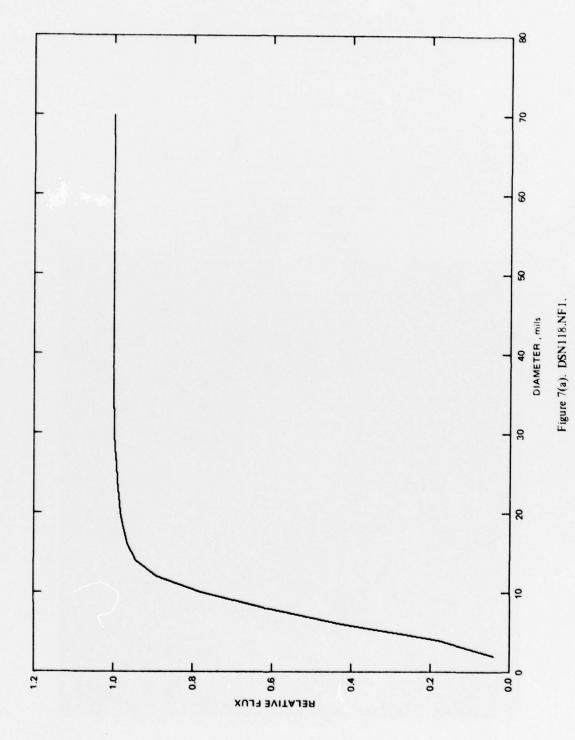


Figure 6(a). DSN118.NF1.



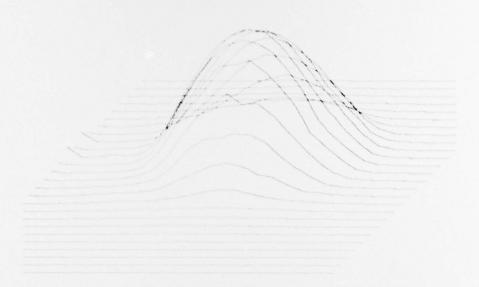


Figure 5(b). DSN119.NF0.

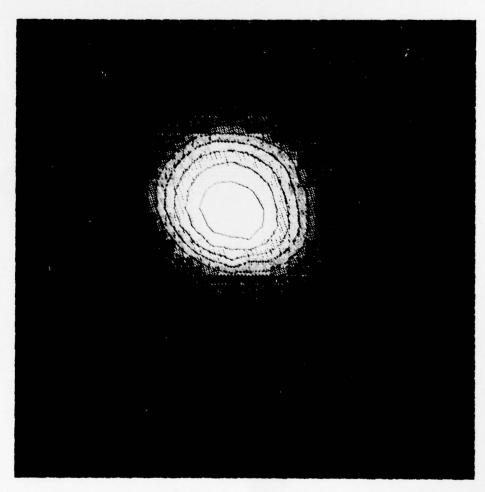


Figure 6(b). DSN119.NF0.

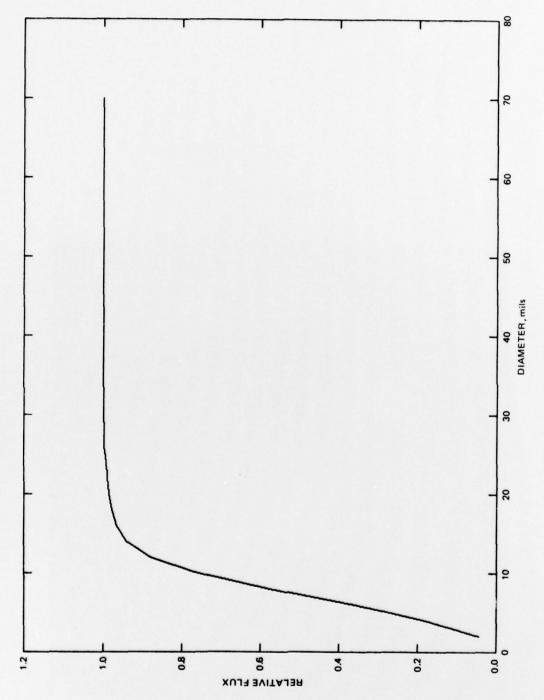


Figure 7(b). DSN119.NF0.

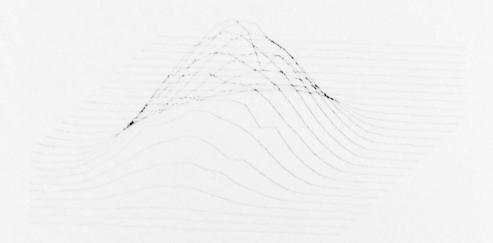


Figure S(c) DSN120 NFO.

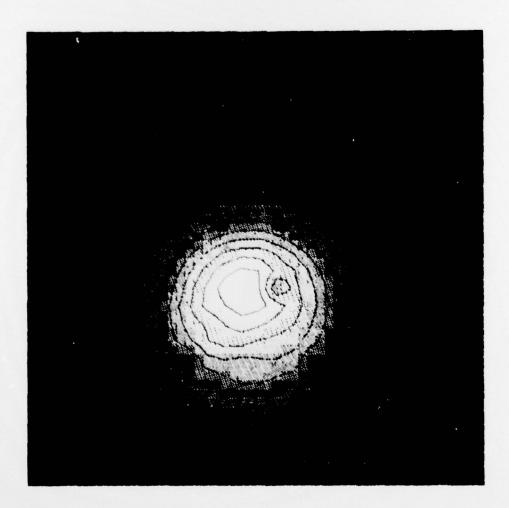
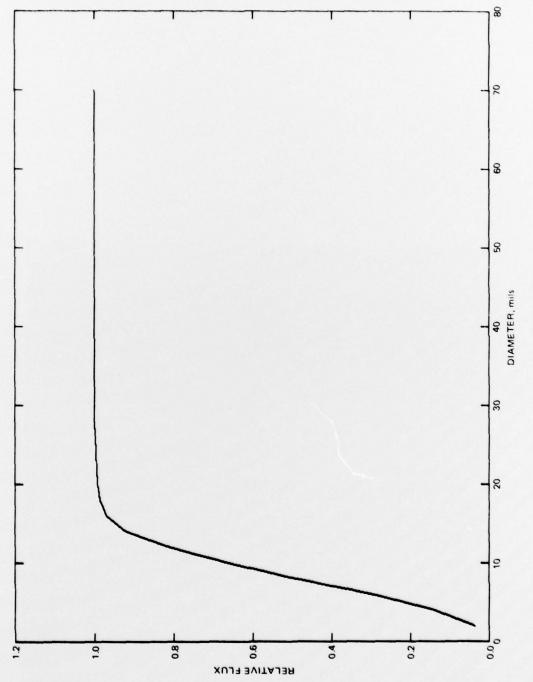


Figure 6(c). DSN120.NF0.



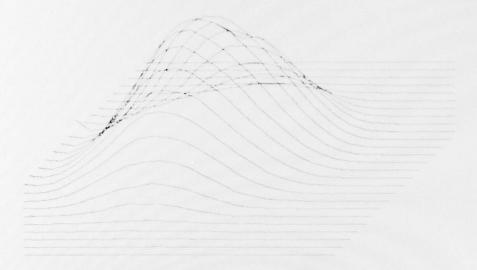


Figure 5(d) DSN121.NF0.

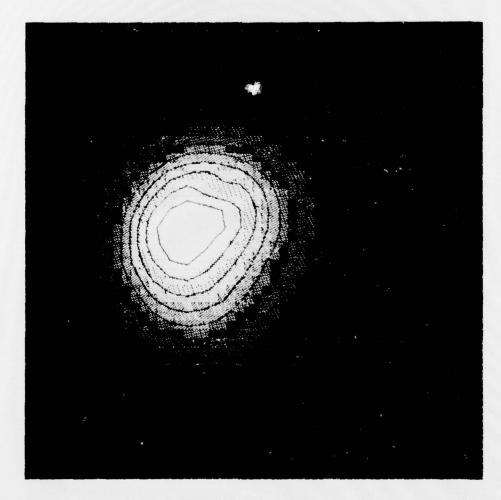


Figure 6(d). DSN121.NF0.

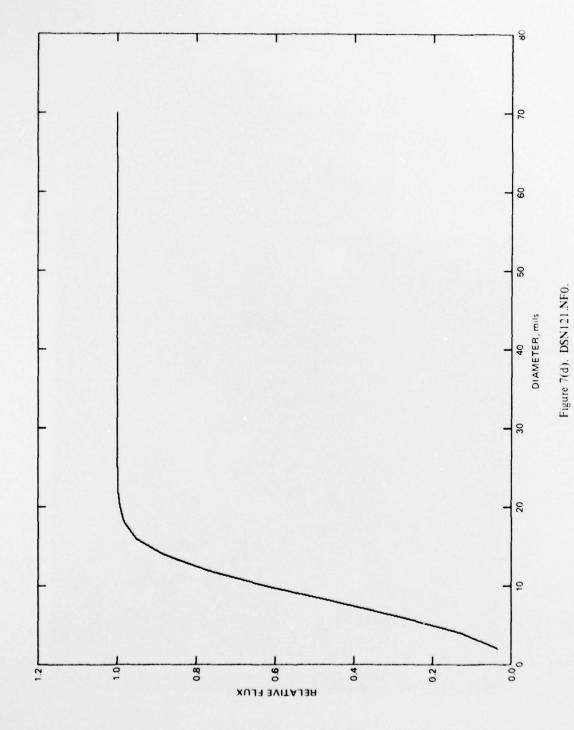




Figure 5(e). DSN122.NF0.

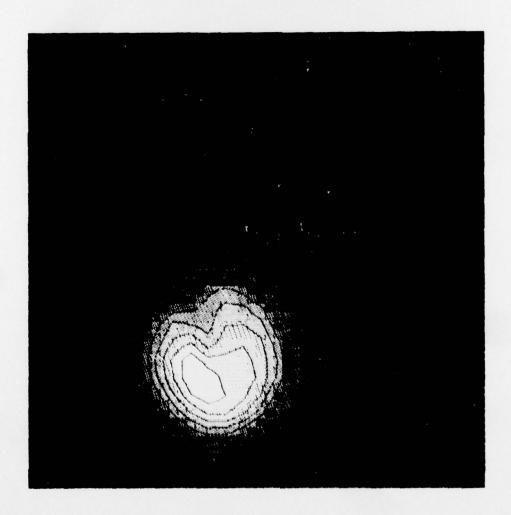
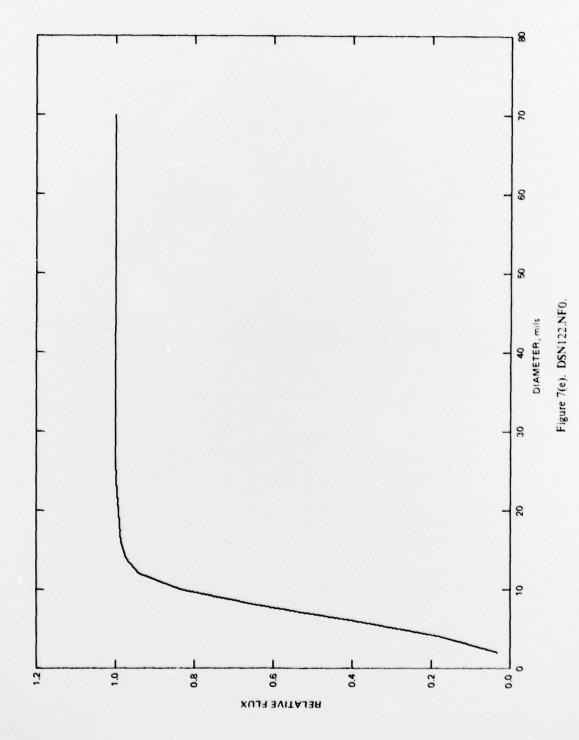


Figure 6(c). DSN122 NF0.



APPENDIX A

GEOMETRY OF THE FAR-FIELD GONIOMETER

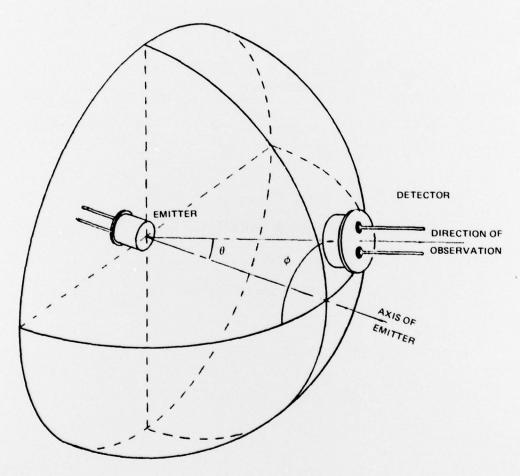


Figure A-1. Geometry of the far-field goniometer.

APPENDIX B

COORDINATE SYSTEM FOR FAR-FIELD GREY SCALE
AND

CONTOUR REPRESENTATIONS

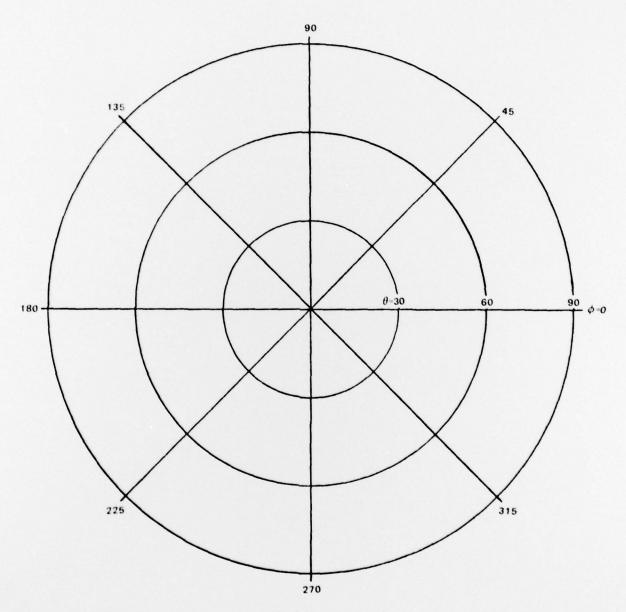


Figure B-1. Coordinate system for far-field grey scale and contour representations.

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